



NAVAL UNDERWATER SYSTEMS CENTER Newport, Rhode Island 02840

Technical Memorandam

COMPUTER AIDED PARAMETRIC SONAR DESIGN UPDATE.

30 October 1073

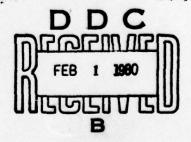
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Prepared by: Edmind C. Januar (10) E. C./Gannon Parametrie Sonar Group

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Digital Computing Division

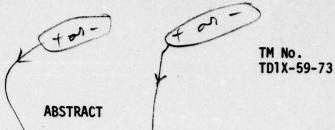
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A computer program was written that simplifies the design of parametric sonars. This program has since been modified to update the calculation for secondary directivity index and to include calculations for secondary beamwidth and primary beamwidth. The tolerance on the determination of secondary source level has been reduced from 1.0 dB to 10.5 dB with a consequent tightening of tolerances on all other related calculated quantities. Finally, a new plotting method has been introduced to give plots in the form of families of curves for ease of design analysis.

ADMINISTRATIVE INFORMATION

This work was prepared under Project No. A-614-19, Principal Investigator, Dr. A. J. Van Woerkum, Code TC.

The authors of this memorandum are located at the New London Laboratory, Naval Underwater Systems Center, New London, Connecticut.

The authors wish to acknowledge Dr. M. B. Moffett for his help.

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Figure No. Title

1 thru 3 PADB Design Curves

4 thru 6 NDIS Design Curves

7 Parametric Sonar Design,

Parametric Sonar Design, Simplified Flow Chart, Updated.

INTRODUCTION

A computer program aimed at automating the design process for parametric sonars was written. $^{\rm I}$ The program allows the designer to work from a known secondary source level (LSS) and a known secondary frequency (F) for a range of values of projector area (A), primary source level per tone (LSP) and a given stepdown ratio (FO/F). The program will build a matrix of possible designs that can be compared to other factors to achieve a workable and realistic design. This computer program is based on the Mellen and Moffett theory. 2

Some new information in the area of directivity index, a tightening of the tolerances on the computed data, and an alternate routine for plotting data have been incorporated into the original program. Since the computer program and its use has been discussed in detail in the earlier memorandum, only the changes and their effects will be taken up in this memorandum.

CHANGES

The program remains basically the same as that discussed in the earlier memorandum. The changes are a result of new information about the directivity, a desire to tighten the tolerances on the computed information, and a need for a plot that arranges the data in the form of a family of curves for ease of analysis.

Directivity Index and 3 dB bandwidth

Investigation has revealed that the original expression for directivity index by Mellen and Moffett 2 does not always predict the secondary frequency directivity index (NDIS) accurately. A new expression was developed by Moffett 3 which was deemed more accurate over the region of concern. This expression is

NDIS = NDIP - 10 LOG
$$(Ye^{-0.65Y(F/F0)^2}+1/2)$$
 (1)

where
$$Y = \pi_X F/[5(GL)(F0)] + 0.685 (AL)(R0)(F0)/F$$
 (2)

F = Secondary Frequency in kHz

FO = Primary Frequency in kHz

NDIP = Primary directivity index in dB

GL = Parametric gain in linear units

 χ = Primary saturation number. ² In this program a table of these numbers is created for use. ¹

AL = Absorption loss in nepers/meter 1

A related term that is now calculable is the secondary frequency 3 dB beamwidth (BWS). This is expressed as

BWS = BWP $\sqrt{Ye^{-0.65Y(F0/F)^2}+1/2}$ deg. (3)

As can be seen from the expression, BWS depends on the primary frequency 3 dB beamwidth (BWP). In this program, BWP is selected as being for a circular piston and this is expressed as

BWP =
$$(3.24) (5.73) \sqrt{4\pi A(F0)^2 (10^3)^2/c^2} deg.$$
 (4)

where C = Sound velocity in meters/second.

The expressions for NDIS and BWS contain an aperture correction originally derived from circular piston theory. However, the expressions are also applicable to square piston projectors. Thus all of the computed information relating to beamwidths and NDIS applies to circular and square piston projectors.

A complete computer printout of a sample example is shown in Appendix A. The sample example is the same one used in reference 1 so that the difference between the new and old programs can be compared. The NDIS column in the output tables now reflects the new theory. Also, two new columns appear, one for BWS and the other for BWP.

Tolerance

In order to solve a given problem, the computer program must compare each calculated value of LSS for each data point against a nominal secondary frequency source level (LSSI) value that is put into the computer in the input data. The tolerance on this comparison was ± 1.0 dB in the old form of the program. The new tolerance is ± 0.5 dB. Thus, the tolerance on all other computed values that depend on LSS is proportionately tighter than under previous conditions. These quantities and their new tolerances are:

G = Parametric Gain ± 0.5 dB,

LSP = Primary Frequency Source Level per tone +0.5 dB,

PADB = Acoustic power per primary frequency +0.5 dB.

The PA which is the acoustic power per primary frequency in watts is also proportionately more accurate, as the ± 0.5 dB tolerance for PADB implies. The new formula for NDIS as well as the formulas for BWS and BWP depend on GL and χ where

GL = antilog (G/20)

and χ is selected from a table of χ values formed by the program according to an equation. Because GL and χ always appear as the ratio $\chi/(GL)$, the tolerances on NDIS, BWS and BWP will never exceed ± 1.0 dB. The tolerances on NDIS, BWS and BWP will vary and depend on the operating point on the Mellen and Moffett² curves.

An equation for determing a table of χ values has been mentioned. This equation determines the increment of χ in a table formed by the program and stored in the computer for use in determining the values of LSS through the use of a numerical integration algorithm by Goldstein. The table is formed such that each next increasing value of χ is a fixed percentage of the previous value. In order to reduce the tolerance on LSS it was necessary to reduce the fixed percentage increase on successive values of χ . The required new formula for χ is

 $x_{(I+1)} = 1.04881 x_{I}$

for 172 values starting from $\chi_0 = 0.00953462$.

New Plots

When it comes to analyzing the results for a given set of design parameters, the single on-line plots of LSS vs FO/F and NDIS vs FO/F for each different combination of secondary frequency (F), area (A) and nominal source level (LSSI) are cumbersome. What has been devised to overcome this shortcoming is plots of LSS vs FO/F and NDIS vs FO/F for a given family of LSS values for each combination of F and A. Figures 1 through 6 show the results of this new plotting method for the sample example of Appendix A. The plots were made on an off-line plotter (Calcomp) that is used with the Univac 1108 computer.

These plots can save many man hours of hand plotting to achieve a similar matrix. Also, the family of curves approach places all of the data for a given F and A on one piece of paper and allows the designer to conveniently view all the available trade-offs. How the new plotting method fits into the computer program flow is shown in Figure 7.

CONCLUSION

A computer program to aid in the design of parametric sonars has been upgraded. The latest information has been incorporated in calculating the secondary frequency directivity index (NDIS). Also two new quantities have been introduced. They are the secondary frequency 3 dB beamwidth (BWS) and the primary frequency 3 dB beamwidth (BWP). These three quantities are valid for a circular and square piston projector.

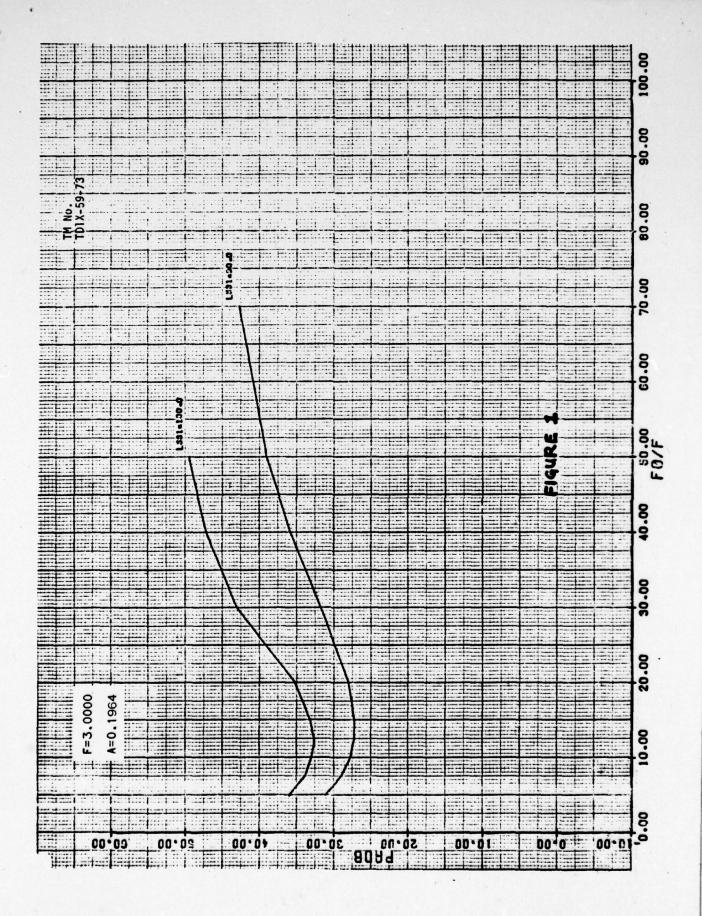
The tolerances on the calculated information have been tightened. Thus, for example, the secondary source level (LSS) can now be computed to ± 0.5 dB.

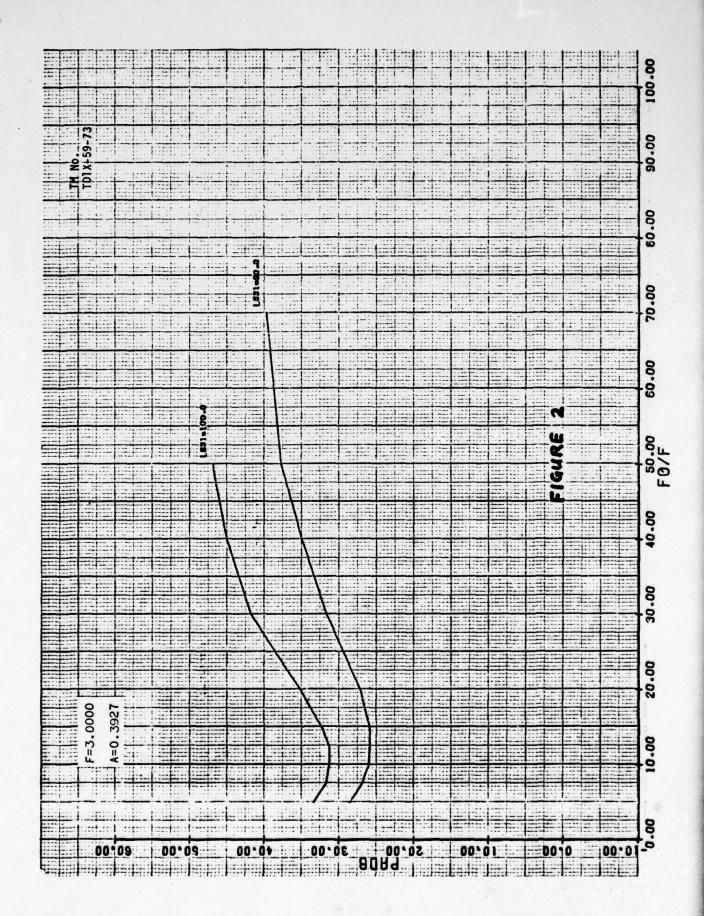
A new plotting method using the family of curves approach is now used. Plots of acoustic power per tone vs downshift ratio (PADB vs FO/F) and secondary directivity index vs downshift ratio (NDIS vs FO/F) can now be made for a family of LSS values for a fixed secondary frequency (F) and a projector area (A). This new type of plot enables the designer to more readily observe trends and to make tradeoffs.

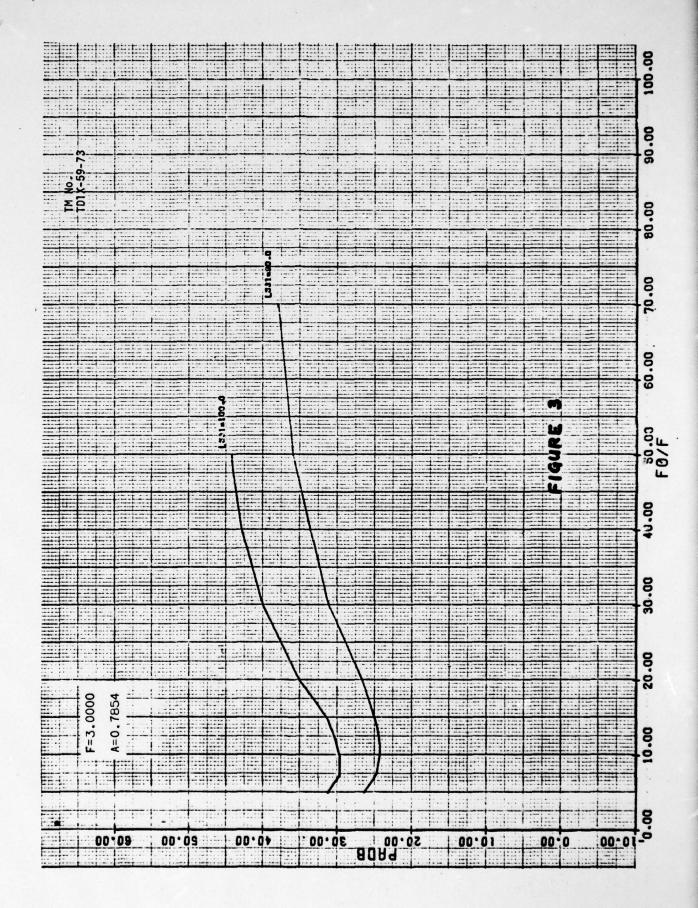
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- 4. Goldstein, M., "On a Numerical Integration in Parametric Sonar Research," NUSC Technical Memorandum No. PA4-268-71, 21 Oct 1971, (Unclassified).

FIGURES 1 THROUGH 3
DESIGN CURVES (PADB VS FO/F)

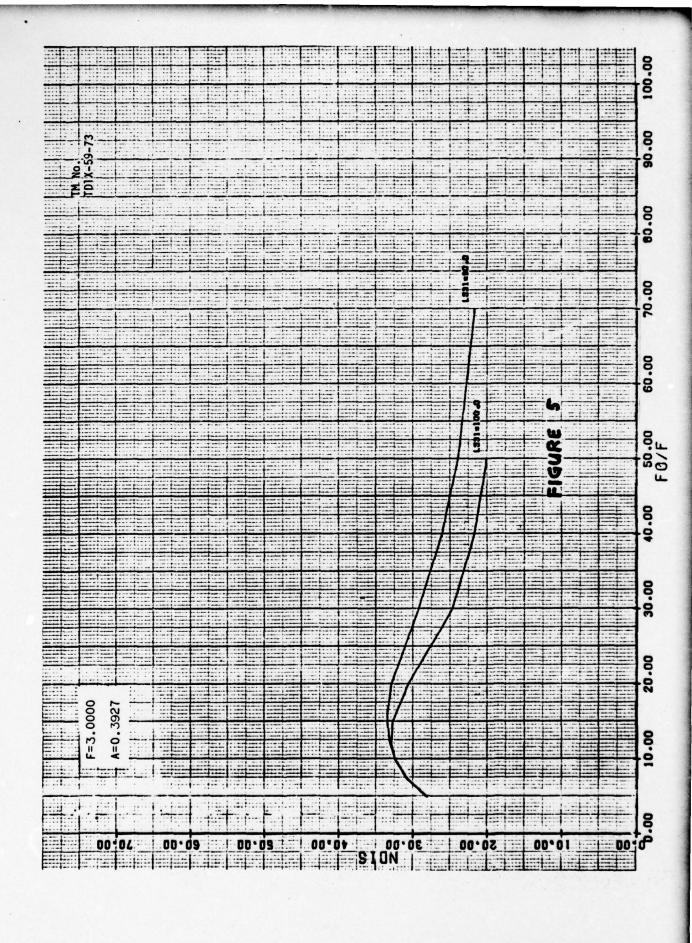






FIGURES 4 THROUGH 6

DESIGN CURVES (NDIS VS FO/F)



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SIMPLIFIED FLOW CHART,

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APPENDIX A

This appendix shows a sample example and the form the tables and on-line plots take as they come out of the computer. The off-line plots were shown in Figures 1 through 6 in the main text.

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TOMORPOOT	TOADDOOR	Topopoport	Topopopor	TOADDADATE	TOMORNOTE		18,000 20,0000 30,0000 40,0000 50,0000 60,0000 70,0000 80,0000	20.000 30.000 40.0000 70.0000 60.0000 70.0000 80.0000	20.000 30.0000 40.0000 70.0000 60.0000 70.0000 80.0000	20.000 30.000 40.0000 70.0000 70.0000 80.0000	25.0000 30.0000 90.0000 90.0000 90.0000 90.0000	25.0000 30.0000 90.0000 90.0000 90.0000	25.0000 30.000	28.0000 30.000	28.0000 30.000	28.0000 30.000	28.0000 30.00000 30.00	20.000 30.000 30.000 30.000 90.000 90.000 90.000	28.0000 30.0000 40.0000 40.0000 40.0000 40.0000	**************************************	DATE 231073 PARE 431073 PARE 4	OATE #33,073 PAGE 99	OATE 23,073 PAGE 49	DATE ESSUES PAGE	DATE ESSOTS PARE 49	OATE E33073 PARE 99
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